# **WIND POWER**

ergy for human use are fossil fuels such as oil, coal, and natural gas. Another important contributor is nuclear energy. All as a function of the ratio  $\lambda$  of the tip speed to the wind speed: these sources produce environmental pollution. Alternatives to them are renewable sources such as solar, ocean waves, and wind energy. In some areas of the world, wind can be an important contributor to electricity production. It gives electric where  $\omega_r$  is the rotor speed and  $\lambda$  is the tip-wind-speed ratio.<br>
from the wind is normally extracted by a wind turbine, which<br>
converts the kinetic p power by use of an electrical generator. Figure 1 shows photo-

wind is not constant. In the other system, the wind-electric that the maximum  $C_p$  can be obtained at only one wind a well-established electricity if the blade tip speed is fixed. generator directly feeds power into a well-established electrical power grid. Here also, if wind-electric is a significant portion of the overall generation, fluctuations in wind speeds **POWER CONTROL METHODS** cause undesirable power system oscillations. To overcome this, energy storage has to be available on a large scale, which **Stall Regulation**<br>is usually not economical. Batteries, superconducting induc-<br>tors, and fuel cells are obvious means, but in general, storage. The most com tors, and fuel cells are obvious means, but in general, storage The most commonly used power control method at higher<br>systems reduce the overall efficiency and cause the price to wind speeds is stall regulation, where the systems reduce the overall efficiency and cause the price to wind speeds is stall regulation, where the rotor profile of the<br>he too high. Another solution, to keep wind-electric generation wind turbine controls the mechani be too high. Another solution, to keep wind-electric generation fairly constant, requires reducing the power production of the position of the rotor profile is always fixed in relation to the wind turbine system by control at high wind speeds. However, windmill, and since the rotor speed is almost fixed (varies this solution is not beneficial for the economy of the wind only  $1\%$  to  $2\%$  due to the slip of the induction generator), the

 $($ <10%) to future energy production because of the necessity Then power is lost and the  $C_p$  value decreases. If the wind of a backbone power source. In some special areas where the turbine is properly designed, stall re of a backbone power source. In some special areas where the energy transportation cost is high, the wind power can be a wind turbine profile can be used to control the maximum significant portion. Typical wind power systems are today in shaft power  $P_{\text{max}}$  according to the equat significant portion. Typical wind power systems are today in the power range of 400–600 kW, but new commercial 1.5 MW<br> *P* systems are on the market now. Wind turbines are also mov-

ing offshore in order to get the maximum power from the wind. Offshore the landscape is flat with high wind speeds.

## **POWER IN THE WIND**

When the wind blows, kinetic energy is stored in it. This energy is transformed to mechanical energy by use of a wind turbine. The transfer function from the wind to the mechanical shaft power  $P_{\rm v}$  in a wind turbine is

$$
P_{\rm v} = \frac{1}{2}Av^3 \rho C_{\rm p} \tag{1}
$$

$$
A = \pi (d/2)^2 \tag{2}
$$

where  $P_{\rm v}$  is the mechanical shaft power (W), *A* is the total area swept by the wind turbine (m<sup>2</sup>),  $d$  is the turbine diameter (m),  $v$  is the wind speed (m/s),  $\rho$  is the mass density of air  $(1.225 \text{ kg/m}^3)$ , and  $C_p$  is the power coefficient for the turbine.

Equation (1) shows that the power in the wind is proportional to the cube of the wind speed.

### **POWER IN A WIND TURBINE**

The only unknown parameter in Eq. (1) is the power coeffi-Energy comes from various sources. The major sources of en-<br>eient  $C_p$  for the turbine. This coefficient is a characteristic of<br>ergy for human use are fossil fuels such as oil, coal, and natu-<br>a specific wind turbine cons

$$
\lambda = \frac{(d/2)\omega_{\rm r}}{v} \tag{3}
$$

converts the kinetic power in the wind to mechanical power, tor is used and connected directly to the grid. Measured  $C_p$ <br>which in many applications again is converted into electrical characteristics for two windmills are which in many applications again is converted into electrical characteristics for two windmills are shown in Fig. 2. The nower by use of an electrical generator. Figure 1 shows photo- measured curves show that  $C_p$  has an graphs of a wind turbine and a whole wind turbine park. of  $0.48-0.5$ . It can be shown theoretically that the absolute There are two basic wind power systems. In a standalone maximum  $C_p$  is 0.59. The  $C_p$  curve is used for power control<br>tem where wind is a dominant source of generation a of a windmill and is an important consideration wh system where wind is a dominant source of generation, a <sup>of a</sup> windmill and is an important consideration when a wind<br>backup source based on diesel engines is needed because the rotor is designed aerodynamically. The  $C_p$ 

power system.<br>In many areas wind power will be a fractional supplement speed exceeds a certain limit, turbulence (stall) will result. In many areas wind power will be a fractional supplement speed exceeds a certain limit, turbulence (stall) will result.<br>10%) to future energy production because of the necessity Then power is lost and the  $C<sub>v</sub>$  value

$$
P_{\text{max}} = C_{\text{p}}(\lambda)P_{\text{v}} = \text{constant} \tag{4}
$$

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**Figure 1.** Photographs of (a) a single wind turbine, (b) a wind turbine farm.

When the generator reaches its power limit at high wind power is again measured as an average over ten minutes. In<br>both stall and pitch control fluctuations occur due to wind speeds, the pitch position is changed so that a fixed mechani-<br>cal power is obtained and thereby also a fixed electrical variations. power. This also reduces the mechanical stress in the system compared to stall regulation. A second effect is that at lower **SIMPLE WIND POWER SYSTEMS** wind velocities the highest possible  $C_p$  value can be obtained all the time. The time is not contained the time of  $\mathbb{F}$  For low power (<1 MW) the cheapest generator on the market

also requires a more complex system to control the pitch. This ator (IG), which can be connected directly to the grid without is traditionally done by a hydraulic system in the windmill any special power and control electronics. For higher power but some systems are also electrically based. A basic control other systems can be preferable because of the requirement to system is shown in Fig. 4, where a control unit adjusts the cool the rotor. The only power electronics needed are thyristor pitch. silicon-controlled rectifiers (SCRs) for limiting the inrush cur-

where  $P_{\text{max}}$  is the maximum allowable shaft power to the elec- The control unit can work in different modes. One mode trical generator. The main benefits of such a control system is based on the measured active power to the grid; a search are that it is simple, cheap, and reliable. Figure 3 shows a algorithm is used in order to get the maximum output power. measured power curve for a stall-regulated 500 kW windmill Another method is to measure the wind speed and use a obtained at different wind speeds. There is only a small over- lookup table to give the pitch angle. It is then possible to obshoot above the 500 kW maximum level. The power is ob- tain more power from the wind over the whole range of tained as an average over ten minutes. speeds. Figure 5 shows a measured power curve for a pitchcontrolled 500 kW windmill.

**Pitch Control** Figure 5 shows that a very constant power is measured at  $\frac{1}{2}$ An alternative method to control the power is pitch control,<br>where the rotor turbine (pitch) changes position continuously.<br>When the stall-controlled windmill of Fig. 3. The<br>power is again measured as an average over ten m

This strategy gives a more flexible control system, but it is widely used: the three-phase squirrel-cage induction gener-



**Figure 2.** Power coefficient curves for two windmills (measured): (a) Nordtank NTK 500/37, (b) Vestas V39.

rent during startup. One alternative is the three-phase synchronous generator (SG), but this generator is very stiff, and without any special damping of wind power fluctuations, which can give problems. The SG is also more expensive than the IG. The most cost-optimal solution at present is therefore a standard four-pole squirrel-cage induction generator with a gearbox. Multipole IGs and SGs can also be used. Figure 6 shows the systems for fixed-speed operation.

Some systems use also an induction generator with pole change, so the windmill can operate at two speeds. This gives a better utilization of the wind, but the generator is more expensive. Different techniques exist to get maximum energy from the wind at a given place in the landscape; in particular, it is not always best to have the highest  $C_p$  value of the turbine and windmill at maximum wind speed. It is better to maximize  $C_p$  at the wind speed that has the highest proba-<br>bility.<br>VESTAS V39.



**Figure 3.** Measured power curve for a stall-regulated windmill: Nordtank NTK 500/37.



**Figure 4.** Pitch-controlled windmill.



VESTAS V39.



generator with gearbox, (b) synchronous generator with gearbox,  $(c)$ 

One of the main problems with windmills is that the induc-<br>tion generator requires reactive nower for magnetization An alternative to the system in Fig. 10 is a doubly wound tion generator requires reactive power for magnetization, An alternative to the system in Fig. 10 is a doubly wound<br>which loads the grid unnecessarily The problem is tradition- induction generator where no brushes are used which loads the grid unnecessarily. The problem is tradition- induction generator where no brushes are used, as shown in ally solved by inserting capacitor banks between the windmill Fig. 11. A variable resistance is put i ally solved by inserting capacitor banks between the windmill and the grid as illustrated in Fig. 7. The rotor resistance causes a strolled by power electronics. The rotor resistance causes a

ments of the grid utility company. In many cases there is only control. The losses in the resistor can be dissipated outside on one capacitor bank, but for new 1.5 MW windmills in Den- the rotor shaft. The power electronics is built into the rotor. mark the requirement is that the power factor should be at Two obvious alternatives to the induction generator sysleast 0.99 over the whole operating region. Therefore a num- tems in Fig. 8 and Fig. 9 are a synchronous generator with ber of capacitor banks are used in high-power applications. the same converters. They are shown in Fig. 12 and Fig. 13. The utility also requires the banks to be disconnected from The synchronous generator offers higher efficiency, but is in the grid if the grid breaks down, to be sure that the windmill general more expensive. However, a degree of freedom exists does not run as a standalone unit.  $\qquad \qquad \text{due to the possibility of controlling the field. For a long time}$ 

# **ADVANCED WIND POWER SYSTEMS**

As mentioned, the maximum  $C_p$  of the wind turbine can only be reached at one point in fixed-speed operation. In order to obtain more energy from the wind, adjustable-speed systems can be used, but they require power electronics.

A number of different topologies are possible when adjustable speed is used. The most promising alternative is a forced-commutated, voltage-source ac–dc–ac converter with an induction generator, which is shown in Fig. 8. Another possibility is a current-source inverter, which has poorer dynamics, as shown in Fig. 9.

Up to 2 MW forced-commutated voltage-source systems are available using modern power electronic devices; currentsource converters are used in very high-power applications. In Fig. 8, the inverter to the grid should not produce any significant harmonic currents. Another system for windmills that has been discussed for many years is based on a doubly fed induction generator (DIG), where the rotor is wound and connected by brushes to the outside world. Figure 10 shows a typical topology where the energy in the rotor is fed back to the grid.

Some of the advantages in this system are that ideally it is possible with a standard 1 MW generator to get 2 MW output without overloading the system, and the speed can be adjusted from synchronous speed upwards. Of course, the gener-**Figure 6.** Fixed-speed windmill generator systems: (a) induction justed from synchronous speed upwards. Of course, the gener-<br>generator with gearbox (b) synchronous generator with gearbox (c) ator has a greater thermal lo induction generator without gearbox. power, and it also operates at higher speed. The reactive power consumption in the stator can be compensated by the dc–ac converter. A transformer is necessary in order to optimize the size of the converter. The disadvantages are the **Disturbances to the Grid** brushes, the wound rotor, and a more complex control

The number of capacitor banks depends on the require- speed variation (e.g.,  $\pm 5\%$ ) and this can be used for power



**Figure 7.** Capacitor banks in a typical windmill installation.



**Figure 8.** Forced-commutated voltagesource ac–dc–ac converter for induction generator.



**Figure 9.** Current-source converter for induction generator.



**Figure 10.** Doubly fed induction generator with ac–dc–ac converter and step-up transformer.



Figure 11. Doubly wound induction generator with variable rotor resistance.





**Figure 12.** Forced-commutated voltagesound ac–dc–ac converter for synchronous generator.

**Figure 13.** Current-source converter for synchronous generator.



**Figure 14.** Multipole permanent-magnet synchronous generator with voltage-source forced-commutated converter.



commutated converter.<br>S. J. Philips, W. L. James, and C. V. Nayer, Power electronic system

attempts have been made to avoid the gearbox because there the U.S. Patent No. 5,083,039, 1992.<br>
are losses (4% or more) in it, and one less component in the system gives higher reliability. In order to avoid the gearbox, a multipole generator is one possibility. Two such machines A. C. Saramourtsis et al., Probabilistic evaluation of the performance are a multiple permanent-magnet synchronous generator of wind-diesel energy systems, IEEE T (MPSG) and a multiple switched-reluctance generator 743–752, 1994. (MSRG). The systems are shown in Fig. 14 and Fig. 15 respec-<br>tively. Ensuing and J. H. R. Enslin, Adaptive control strategies<br>for variable-speed doubly-fed wind power generation systems. In

plexity of the windings and the size of the generator. A major 545–552. drawback with the MSRG is the high reactive current, which K. Uhlen, B. A. Foss and O. B. Gjøsøter, Robust control and analysis leads to extra losses. Readers interested in these topics may of a wind-diesel hybrid power plant, *IEEE Trans. Energy Convers.,* refer to the Bibliography.

- B. S. Borowy and Z. M. Salameh, Optimum photovoltaic array size M. Yamamoto and O. Motoyoshi, Active and reactive power control for a hybrid wind/pv system, IEEE Trans. Energy Convers., 9:482- for doubly-fed wound rotor in 488, 1994. *Power Electron.,* **6**: 1991, pp. 624–629.
- B. K. Bose and M. G. Simões, Fuzzy logic based intelligent control of a variable speed cage machine wind generation system. *IEEE Power* FREDE BLAABJERG *Electronics Specialists Conf.,* 1995, pp. 389–395. Aalborg University
- C. Brothers et al., Harmonics on wind/diesel grids, *Wind Eng.*, 17 NED MOHAN (6): 323-331. Iniversity of
- C. Brune, R. Spée, and A. K. Wallace, Experimental evaluation of a variable-speed, doubly-fed wind-power generation system. *IEEE Conf. Record Ind. Applications Soc. Annu. Meet.,* 1993, p. 480–487.
- J. Douglas, Renewables on the rise, *EPRI J.,* 16–25, 1991.
- J. H. R. Enslin and J. D. Van Wyk, A study of a wind power converter with microcomputer based maximal power control utilising an over-synchronous electronic scherbius cascade, *Renewable Energy,* **2** (6): 551–562, 1992.
- P. L. Fraenkel, The development of wind-pumps, *Int. J. Solar Energy,* **14**: 239–255, 1994.
- J. I. Herrera, T. W. Reddock, and J. S. Lawler, Harmonics generated by two variable speed wind generating systems, *IEEE Trans. Energy Convers.,* **3**: 267–273, 1988.
- R. M. Hilloowala and A. M. Sharaf, Modelling, simulation and analysis of variable speed constant frequency wind energy conversion scheme using self excited induction generator. *IEEE Southeastern Symp. Syst. Theor.,* 1991, pp. 33–38.
- R. M. Hilloowala and A. M. Sharaf, A utility interactive wind energy conversion scheme with an asynchronous dc link using a supplementary control loop, *IEEE Trans. Energy Convers.,* **9**: 558–563, 1994.
- T. A. Lipo, Variable speed generator technology options for wind turbine generation, *WEMPEC Summary Publ.,* **2**: 214–220, 1991.
- H. L. Nakra and B. Dubé, Slip power recovery induction generators for large vertical axis wind turbines, *IEEE Trans. Energy Convers.,* **3**: 1988, pp. 733–737.
- P. Novak et al., Modelling and control af variable-speed wind-turbine drive-system dynamics, *IEEE Control Syst.,* **15** (4): 28–38, 1995.
- M. Papadopoulos and P. Malatestas, Operational advantages from the use of ac/dc/ac interface for the connection of wind turbines in diesel power systems. *Eur. Community Wind Energy Conf.,* 1990, pp. 586–590.
- M. P. Papadopoulus and L. Papathanassiou, DQ modelling of a variable speed wind turbine equipped with a double output induction generator. *Stockholm Power Tech. Conf.,* 1995, pp. 194–199. **Figure 15.** Multipole switched-reluctance generator with forced
	- optimisation for remote area mini grid diesel systems. *IEEE IECON '90,* 1990, pp. 1029–1033.
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	- for variable-speed doubly-fed wind power generation systems. In Major problems with multipole generators include the com- *Proc. 1994 IEEE Ind. Appl. Soc. Annu. Meet.,* vol. 1, 1994, pp.
		-
- L. Xu and Y. Tang, A novel wind-power generating system using field orientation controlled doubly-excited brushless reluctance ma-**BIBLIOGRAPHY** chine. In *Proc. 1992 IEEE Ind. Appl. Soc. Annu. Meet.,* 1992, pp. 408–413.
	- for doubly-fed wound rotor induction generator, *IEEE Trans.*

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