

# Material indices

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## Introduction

The performance,  $p$ , of a component is measured by a performance equation. The performance equation contains groups of material properties. These groups are the material indices. Sometimes the 'group' is a single property; thus if the performance of a beam is measured by its stiffness, the performance equation contains only one property, the elastic modulus  $E$ . It is the material index for this problem. More commonly the performance equation contains a group of two or more properties. Familiar examples are the specific stiffness,  $E/\rho$ , and the specific strength,  $\sigma_y/\rho$ , (where  $E$  is Young's modulus,  $\sigma_y$  is the yield strength or elastic limit, and  $\rho$  is the density), but there are many others. They are a key to the optimal selection of materials. Details of the method, with numerous examples are given in references [1] and [2]. PC-based software systems [3] which implement the method are available. This Appendix compiles indices for a range of common applications.

## Uses of material indices

### Material selection

Components have functions: to carry loads safely, to transmit heat, to store energy, to insulate, and so forth. Each function has an associated material index. Materials with high values of the appropriate index maximize that aspect of the performance of the component. For reasons given in reference [1], the material index is generally independent of the details of the design. Thus the indices for beams in the tables which follow are independent of the detailed shape of the beam; that for minimizing thermal distortion of precision instruments is independent of the configuration of the instrument. This gives them great generality.

### Material deployment or substitution

A new material will have potential application in functions for which its indices have unusually high values. Fruitful applications for a new material can be identified by evaluating its indices and comparing these with those of incumbent materials. Similar reasoning points the way to identifying viable substitutes for an incumbent material in an established application.

**Table B1** Stiffness-limited design at minimum mass (cost, energy, environmental impact\*)

<i>Function and constraints*</i>	<i>Maximize</i> <sup>†</sup>
<b>Tie (tensile strut)</b> stiffness, length specified; section area free	$E/\rho$
<b>Shaft (loaded in torsion)</b> stiffness, length, shape specified, section area free	$G^{1/2}/\rho$
stiffness, length, outer radius specified; wall thickness free	$G/\rho$
stiffness, length, wall-thickness specified; outer radius free	$G^{1/3}/\rho$
<b>Beam (loaded in bending)</b> stiffness, length, shape specified; section area free	$E^{1/2}/\rho$
stiffness, length, height specified; width free	$E/\rho$
stiffness, length, width specified; height free	$E^{1/3}/\rho$
<b>Column (compression strut, failure by elastic buckling)</b> buckling load, length, shape specified; section area free	$E^{1/2}/\rho$
<b>Panel (flat plate, loaded in bending)</b> stiffness, length, width specified, thickness free	$E^{1/3}/\rho$
<b>Plate (flat plate, compressed in-plane, buckling failure)</b> collapse load, length and width specified, thickness free	$E^{1/3}/\rho$
<b>Cylinder with internal pressure</b> elastic distortion, pressure and radius specified; wall thickness free	$E/\rho$
<b>Spherical shell with internal pressure</b> elastic distortion, pressure and radius specified, wall thickness free	$E/(1 - \nu)\rho$

\*To minimize cost, use the above criteria for minimum weight, replacing density  $\rho$  by  $C_m\rho$ , where  $C_m$  is the material cost per kg. To minimize energy content, use the above criteria for minimum weight replacing density  $\rho$  by  $q\rho$  where  $q$  is the energy content per kg. To minimize environmental impact, replace density  $\rho$  by  $I_e\rho$  instead, where  $I_e$  is the eco-indicator value for the material (references [1] and [4]).

<sup>†</sup> $E$  = Young's modulus for tension, the flexural modulus for bending or buckling;  $G$  = shear modulus;  $\rho$  = density,  $q$  = energy content/kg;  $I_e$  = eco-indicator value/kg.

**Table B2** Strength-limited design at minimum mass (cost, energy, environmental impact\*)

<i>Function and constraints</i> * <sup>‡</sup>	<i>Maximize</i> <sup>†</sup>
<b>Tie (tensile strut)</b> stiffness, length specified; section area free	$\sigma_f / \rho$
<b>Shaft (loaded in torsion)</b> load, length, shape specified, section area free	$\sigma_f^{2/3} / \rho$
load, length, outer radius specified; wall thickness free	$\sigma_f / \rho$
load, length, wall-thickness specified; outer radius free	$\sigma_f^{1/2} / \rho$
<b>Beam (loaded in bending)</b> load, length, shape specified; section area free	$\sigma_f^{2/3} / \rho$
load length, height specified; width free	$\sigma_f / \rho$
load, length, width specified; height free	$\sigma_f^{1/2} / \rho$
<b>Column (compression strut)</b> load, length, shape specified; section area free	$\sigma_f / \rho$
<b>Panel (flat plate, loaded in bending)</b> stiffness, length, width specified, thickness free	$\sigma_f^{1/2} / \rho$
<b>Plate (flat plate, compressed in-plane, buckling failure)</b> collapse load, length and width specified, thickness free	$\sigma_f^{1/2} / \rho$
<b>Cylinder with internal pressure</b> elastic distortion, pressure and radius specified; wall thickness free	$\sigma_f / \rho$
<b>Spherical shell with internal pressure</b> elastic distortion, pressure and radius specified, wall thickness free	$\sigma_f / \rho$
<b>Flywheels, rotating discs</b> maximum energy storage per unit volume; given velocity	$\rho$
maximum energy storage per unit mass; no failure	$\sigma_f / \rho$

\*To minimize cost, use the above criteria for minimum weight, replacing density  $\rho$  by  $C_m \rho$ , where  $C_m$  is the material cost per kg. To minimize energy content, use the above criteria for minimum weight replacing density  $\rho$  by  $q \rho$  where  $q$  is the energy content per kg. To minimize environmental impact, replace density  $\rho$  by  $I_e \rho$  instead, where  $I_e$  is the eco-indicator value for the material (references [1] and [4]).

<sup>†</sup> $\sigma_f$  = failure strength (the yield strength for metals and ductile polymers, the tensile strength for ceramics, glasses and brittle polymers loaded in tension; the flexural strength or modulus of rupture for materials loaded in bending);  $\rho$  = density.

<sup>‡</sup>For design for infinite fatigue life, replace  $\sigma_f$  by the endurance limit  $\sigma_e$ .

**Table B3** Strength-limited design: springs, hinges etc. for maximum performance\*

<i>Function and constraints</i> <sup>*‡</sup>	<i>Maximize</i> <sup>†</sup>
<b>Springs</b>	
maximum stored elastic energy per unit volume; no failure	$\sigma_f^2/E$
maximum stored elastic energy per unit mass; no failure	$\sigma_f^2/E\rho$
<b>Elastic hinges</b>	
radius of bend to be minimized (max flexibility without failure)	$\sigma_f/E$
<b>Knife edges, pivots</b>	
minimum contact area, maximum bearing load	$\sigma_f^3/E^2$ and $H$
<b>Compression seals and gaskets</b>	
maximum conformability; limit on contact pressure	$\sigma_f^{3/2}/E$ and $1/E$
<b>Diaphragms</b>	
maximum deflection under specified pressure or force	$\sigma_f^{3/2}/E$
<b>Rotating drums and centrifuges</b>	
maximum angular velocity; radius fixed; wall thickness free	$\sigma_f/\rho$

\*To minimize cost, use the above criteria for minimum weight, replacing density  $\rho$  by  $C_m\rho$ , where  $C_m$  is the material cost per kg. To minimize energy content, use the above criteria for minimum weight replacing density  $\rho$  by  $q\rho$  where  $q$  is the energy content per kg. To minimize environmental impact, replace density  $\rho$  by  $I_e\rho$  instead, where  $I_e$  is the eco-indicator value for the material (references [1] and [4]).

<sup>†</sup> $\sigma_f$  = failure strength (the yield strength for metals and ductile polymers, the tensile strength for ceramics, glasses and brittle polymers loaded in tension; the flexural strength or modulus of rupture for materials loaded in bending);  $\rho$  = density;  $H$  = hardness.

<sup>‡</sup>For design for infinite fatigue life, replace  $\sigma_f$  by the endurance limit  $\sigma_e$ .

**Table B4** Vibration-limited design

<i>Function and constraints</i>	<i>Maximize</i> <sup>*</sup>
<b>Ties, columns</b>	
maximum longitudinal vibration frequencies	$E/\rho$
<b>Beams, all dimensions prescribed</b>	
maximum flexural vibration frequencies	$E/\rho$
<b>Beams, length and stiffness prescribed</b>	
maximum flexural vibration frequencies	$E^{1/2}/\rho$
<b>Panels, all dimensions prescribed</b>	
maximum flexural vibration frequencies	$E/\rho$
<b>Panels, length, width and stiffness prescribed</b>	
maximum flexural vibration frequencies	$E^{1/3}/\rho$
<b>Ties, columns, beams, panels, stiffness prescribed</b>	
minimum longitudinal excitation from external drivers, ties	$\eta E/\rho$
minimum flexural excitation from external drivers, beams	$\eta E^{1/2}/\rho$
minimum flexural excitation from external drivers, panels	$\eta E^{1/3}/\rho$

\* $E$  = Young's modulus for tension, the flexural modulus for bending;  $G$  = shear modulus;  $\rho$  = density;  $\eta$  = damping coefficient (loss coefficient).

Table B5 Damage-tolerant design

<i>Function and constraints</i>	<i>Maximize*</i>
<b>Ties (tensile member)</b>	
Maximize flaw tolerance and strength, load-controlled design	$K_{Ic}$ and $\sigma_f$
Maximize flaw tolerance and strength, displacement-control	$K_{Ic}/E$ and $\sigma_f$
Maximize flaw tolerance and strength, energy-control	$K_{Ic}^2/E$ and $\sigma_f$
<b>Shafts (loaded in torsion)</b>	
Maximize flaw tolerance and strength, load-controlled design	$K_{Ic}$ and $\sigma_f$
Maximize flaw tolerance and strength, displacement-control	$K_{Ic}/E$ and $\sigma_f$
Maximize flaw tolerance and strength, energy-control	$K_{Ic}^2/E$ and $\sigma_f$
<b>Beams (loaded in bending)</b>	
Maximize flaw tolerance and strength, load-controlled design	$K_{Ic}$ and $\sigma_f$
Maximize flaw tolerance and strength, displacement-control	$K_{Ic}/E$ and $\sigma_f$
Maximize flaw tolerance and strength, energy-control	$K_{Ic}^2/E$ and $\sigma_f$
<b>Pressure vessel</b>	
Yield-before-break	$K_{Ic}/\sigma_f$
Leak-before-break	$K_{Ic}^2/\sigma_f$

\* $K_{Ic}$  = fracture toughness;  $E$  = Young's modulus;  $\sigma_f$  = failure strength (the yield strength for metals and ductile polymers, the tensile strength for ceramics, glasses and brittle polymers loaded in tension; the flexural strength or modulus of rupture for materials loaded in bending).

Table B6 Thermal and thermo-mechanical design

<i>Function and constraints</i>	<i>Maximize*</i>
<b>Thermal insulation materials</b>	
minimum heat flux at steady state; thickness specified	$1/\lambda$
minimum temp rise in specified time; thickness specified	$1/a = \rho C_p/\lambda$
minimize total energy consumed in thermal cycle (kilns, etc)	$\sqrt{a}/\lambda = \sqrt{1/\lambda \rho C_p}$
<b>Thermal storage materials</b>	
maximum energy stored/unit material cost (storage heaters)	$C_p/C_m$
maximize energy stored for given temperature rise and time	$\lambda/\sqrt{a} = \sqrt{\lambda \rho C_p}$
<b>Precision devices</b>	
minimize thermal distortion for given heat flux	$\lambda/\alpha$
<b>Thermal shock resistance</b>	
maximum change in surface temperature; no failure	$\sigma_f/E\alpha$
<b>Heat sinks</b>	
maximum heat flux per unit volume; expansion limited	$\lambda/\Delta\alpha$
maximum heat flux per unit mass; expansion limited	$\lambda/\rho\Delta\alpha$
<b>Heat exchangers (pressure-limited)</b>	
maximum heat flux per unit area; no failure under $\Delta p$	$\lambda\sigma_f$
maximum heat flux per unit mass; no failure under $\Delta p$	$\lambda\sigma_f/\rho$

\* $\lambda$  = thermal conductivity;  $a$  = thermal diffusivity;  $C_p$  = specific heat capacity;  $C_m$  = material cost/kg;  $T_{max}$  = maximum service temperature;  $\alpha$  = thermal expansion coeff.;  $E$  = Young's modulus;  $\rho$  = density;  $\sigma_f$  = failure strength (the yield strength for metals and ductile polymers, the tensile strength for ceramics, glasses and brittle polymers).

**Table B7** Electro-mechanical design

<i>Function and constraints</i>	<i>Maximize*</i>
<b>Bus bars</b>	
minimum life-cost; high current conductor	$1/\rho_e \rho C_m$
<b>Electro-magnet windings</b>	
maximum short-pulse field; no mechanical failure	$\sigma_y$
maximize field and pulse-length, limit on temperature rise	$C_p \rho / \rho_e$
<b>Windings, high-speed electric motors</b>	
maximum rotational speed; no fatigue failure	$\sigma_e / \rho_e$
minimum ohmic losses; no fatigue failure	$1/\rho_e$
<b>Relay arms</b>	
minimum response time; no fatigue failure	$\sigma_e / E \rho_e$
minimum ohmic losses; no fatigue failure	$\sigma_e^2 / E \rho_e$

\* $C_m$  = material cost/kg;  $E$  = Young's modulus;  $\rho$  = density;  $\rho_e$  = electrical resistivity;  $\sigma_y$  = yield strength;  $\sigma_e$  = endurance limit.

## References

Derivations for almost all the indices listed in this Appendix can be found in references [1] and [2].

- [1] Ashby, M.F. (1999) *Materials Selection in Mechanical Design*, 2nd edn, Chapter 6, Butterworth-Heinemann, Oxford.
- [2] Ashby, M.F. and Cebon, D. (1995) *Case Studies in Materials Selection*, Granta Design, Trumpington.
- [3] CMS 2.1(1995) and CMS 3.0 (1999) Granta Design, Trumpington.
- [4] Goedkoop, M.J., Demmers, M. and Collignon, M.X. 'Eco-Indicator '95, Manual', Pré Consultants, and the Netherlands Agency for Energy and the Environment, Amersfort, Holland (1995).