

8.1-1

$$L^2 = \underline{Y} \cdot \underline{Y} = [u' v' w'] \begin{Bmatrix} u' \\ v' \\ w' \end{Bmatrix} = \{d'\}^T \{d'\}$$

$$L^2 = ([\underline{\Lambda}] \{d\})^T ([\underline{\Lambda}] \{d\}). \text{ Also, } L = \{d\}^T \{d\}.$$

$$\{d\}^T [\underline{\Lambda}]^T [\underline{\Lambda}] \{d\} = \{d\}^T \{d\}, \text{ or}$$

$$\{d\}^T ([\underline{\Lambda}]^T [\underline{\Lambda}] - [\underline{\Xi}]) \{d\} = 0.$$

Must be true for any $\{d\}$, so

$$[\underline{\Lambda}]^T [\underline{\Lambda}] = [\underline{\Xi}]. \text{ From Eq. 8.1-1, this}$$

$$\text{means } \sum l_i^2 = \sum m_i^2 = \sum n_i^2 = 1$$

$$\text{and } \sum l_i m_i = \sum m_i n_i = \sum n_i l_i = 0$$

8. 1-2

$$[\underline{\Lambda}] = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$[\underline{\Lambda}] = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

8.2-1

$$[\underline{E}'] = \frac{E}{1-\nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{bmatrix}$$

We can ignore the common multiplier $E/(1-\nu^2)$ in the following. The product $[\underline{T}_\epsilon]^T [\underline{E}'] [\underline{T}_\epsilon]$ is found to be symmetric, with the following terms in its upper triangle. Let $c = \cos \theta$, $s = \sin \theta$.

$$(1,1) = c^4 + \nu c^2 s^2 + \nu c^2 s^2 + s^4 + 2c^2 s^2 - 2\nu c^2 s^2 \\ = (c^2 + s^2)^2 = 1$$

$$(1,2) = c^2 s^2 + \nu c^4 + \nu s^4 + c^2 s^2 - 2c^2 s^2 + 2\nu c^2 s^2 \\ = \nu (c^2 + s^2)^2 = \nu$$

$$(1,3) = c^3 s (1-\nu) + c s^3 (\nu-1) - (1-\nu)(c^3 s - c s^3) \\ = 0$$

$$(2,2) = s^4 + \nu c^2 s^2 + \nu c^2 s^2 + c^4 + 2c^2 s^2 (1-\nu) \\ = (c^2 + s^2)^2 = 1$$

$$(2,3) = c s^3 (1-\nu) + c^3 s (\nu-1) + (1-\nu)(c^3 s - c s^3) \\ = 0$$

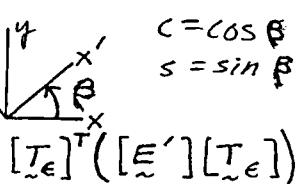
$$(3,3) = c^2 s^2 (1-\nu) + c^2 s^2 (1-\nu) + \frac{1-\nu}{2} (c^2 - s^2)^2 \\ = \frac{1-\nu}{2} (c^2 + s^2)^2 = \frac{1-\nu}{2}$$

So, after restoring the multiplier

$E/(1-\nu^2)$, we obtain $[\underline{E}] = [\underline{E}']$.

8.2-2

$$[\underline{\underline{E}}'] = \begin{bmatrix} E_a & 0 & 0 \\ 0 & E_b & 0 \\ 0 & 0 & G \end{bmatrix}$$



$$c = \cos \beta$$

$$s = \sin \beta$$

$$\begin{bmatrix} c^2 & s^2 & -2cs \\ s^2 & c^2 & 2cs \\ cs & -cs & c^2-s^2 \end{bmatrix} \begin{bmatrix} c^2 E_a & s^2 E_a & cs E_a \\ s^2 E_b & c^2 E_b & -cs E_b \\ -2cs G & 2cs G & G(c^2-s^2) \end{bmatrix} = [\underline{\underline{E}}]$$

$$E_{11} = c^4 E_a + s^4 E_b + 4c^2 s^2 G$$

$$E_{12} = c^2 s^2 (E_a + E_b) - 4c^2 s^2 G = E_{21}$$

$$E_{13} = c^3 s E_a - c s^3 E_b - 2cs(c^2-s^2)G = E_{31}$$

$$E_{22} = s^4 E_a + c^4 E_b + 4c^2 s^2 G$$

$$E_{23} = c s^3 E_a - c^3 s E_b + 2cs(c^2-s^2)G = E_{32}$$

$$E_{33} = c^2 s^2 (E_a + E_b) + G(c^2-s^2)^2$$

$$\text{For } \beta = 0, [\underline{\underline{E}}] = [\underline{\underline{E}}']$$

$$\text{For } \beta = \pi/2, E_{11} = E_b, E_{22} = E_a, E_{33} = G, \text{ remainder of } [\underline{\underline{E}}] \text{ null.}$$

8.2-3

$$[\underline{T}_\epsilon]^T [\underline{T}_\epsilon] = \begin{bmatrix} c^4 + s^4 + 4c^2s^2 & \dots \\ \vdots & \ddots \end{bmatrix}$$

$$c^4 + s^4 + 4c^2s^2 = (c^2 + s^2)^2 + 2c^2s^2 = 1 + c^2s^2$$

Unity only if $c^2s^2 = 0$; not so for all β .

Hence $[\underline{T}_\epsilon]^T [\underline{T}_\epsilon] \neq [\underline{I}]$; $[\underline{T}_\epsilon]$ not orthogonal.

8.3-1

$$\text{For d.o.f. } u_1 \neq u_2, [\underline{k}'] = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$u_r = u_2 - u_1, \quad u_2 = u_1 + u_r$$

$$\begin{Bmatrix} u_1 \\ u_2 \end{Bmatrix} = \underbrace{\begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix}}_{[\underline{I}]} \begin{Bmatrix} u_1 \\ u_r \end{Bmatrix} \quad [\underline{I}] [\underline{k}'] = \frac{AE}{L} \begin{bmatrix} 0 & -1 \\ 0 & 1 \end{bmatrix}$$

$$[\underline{I}]^T ([\underline{k}'] [\underline{I}]) = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \frac{AE}{L} \begin{bmatrix} 0 & -1 \\ 0 & 1 \end{bmatrix} = \frac{AE}{L} \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}$$

8.3-2

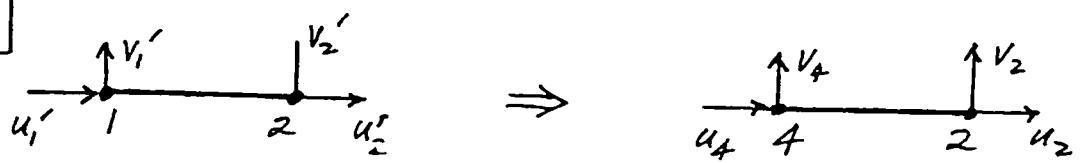
$$u = \underline{N}' \{\underline{d}'\} = \begin{bmatrix} \frac{-3+\sqrt{3}}{2} & 1-\sqrt{3} & \frac{3+\sqrt{3}}{2} \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix}$$

$$\begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 1/2 & 1 & 1/2 \\ 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_r \\ u_3 \end{Bmatrix} \quad \text{or } \{\underline{d}'\} = [\underline{I}] \{\underline{d}\}$$

$$u = \underline{N}' [\underline{I}] \{\underline{d}\} \quad \text{or} \quad u = \underline{N} \{\underline{d}\} \quad \text{where}$$

$$\begin{aligned} \underline{N} &= \underline{N}' [\underline{I}] = \begin{bmatrix} \frac{-3+\sqrt{3}^2+1-\sqrt{3}^2}{2} & 1-\sqrt{3} & \frac{1-\sqrt{3}^2+\sqrt{3}+\sqrt{3}^2}{2} \end{bmatrix} \\ &= \begin{bmatrix} \frac{1-\sqrt{3}}{2} & 1-\sqrt{3} & \frac{1+\sqrt{3}}{2} \end{bmatrix} \end{aligned}$$

8.3-3



$$\begin{Bmatrix} u'_1 \\ v'_1 \\ u'_2 \\ v'_2 \end{Bmatrix} = \underbrace{\begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \end{bmatrix}}_{[T]} \begin{Bmatrix} u_1 \\ v_1 \\ u_2 \\ u_4 \\ v_2 \\ v_4 \end{Bmatrix}$$

8.4-1

Set $u_1 = v_1 = u_2 = v_2 = 0$, but temporarily retain u_4 . $\{\underline{K}'\} \{R'\} = \{\underline{R}'\}$ is

$$k \begin{bmatrix} \frac{3}{2} & \frac{1}{2} & -\frac{1}{2} & -\frac{1}{2} \\ \frac{1}{2} & \frac{1}{2} & -\frac{1}{2} & -\frac{1}{2} \\ -\frac{1}{2} & -\frac{1}{2} & \frac{1}{2} & \frac{1}{2} \\ -\frac{1}{2} & -\frac{1}{2} & \frac{1}{2} & \frac{3}{2} \end{bmatrix} \begin{Bmatrix} u_3 \\ v_3 \\ u_4 \\ v_4 \end{Bmatrix} = \begin{Bmatrix} R_{x3} \\ R_{y3} \\ R_{x4} \\ -P \end{Bmatrix}$$

Now set

$u_4 = 0$:

discard

row 4

col. 3

$$\frac{k}{2} \begin{bmatrix} 3 & 1 & -1 \\ 1 & 1 & -1 \\ -1 & -1 & 3 \end{bmatrix} \begin{Bmatrix} u_3 \\ v_3 \\ v_4 \end{Bmatrix} = \begin{Bmatrix} R_{x3} \\ R_{y3} \\ -P \end{Bmatrix}, \begin{bmatrix} I \\ I \\ I \end{bmatrix} = \begin{bmatrix} 0.8 & 0.6 & 0 \\ -0.6 & 0.8 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\underbrace{[I]^T ([\underline{K}'] [I])}_{\downarrow} = \begin{bmatrix} 0.8 & -0.6 & 0 \\ 0.6 & 0.8 & 0 \\ 0 & 0 & 1 \end{bmatrix} \frac{k}{2} \begin{bmatrix} 1.8 & 2.6 & -1 \\ 0.2 & 1.4 & -1 \\ -0.2 & -1.4 & 3 \end{bmatrix}$$

$$\frac{k}{2} \begin{bmatrix} 1.32 & 1.24 & -0.2 \\ 1.24 & 2.68 & -1.4 \\ -0.2 & -1.4 & 3.0 \end{bmatrix} \begin{Bmatrix} u_3 \\ v_3 \\ v_4 \end{Bmatrix} = \begin{Bmatrix} 0 \\ R_3 \\ -P \end{Bmatrix}$$

Set $V_3 = 0$,

solve for

U_3 & v_4 .

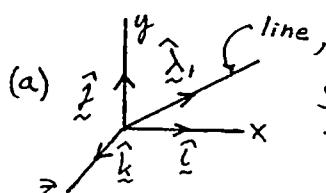
$$1.32 U_3 - 0.2 v_4 = 0, \quad U_3 = -0.102 P/k$$

$$-0.2 U_3 + 3.0 v_4 = -2P/k, \quad v_4 = -0.673 P/k$$

$$F_{t-3} = \left| k (v_3 \cos \beta) \right| = k (0.102 \frac{P}{k}) (0.8) = 0.0816 P$$

(tension)

8.4-2

(a)  line, $\hat{\lambda}_1 = l_1 \hat{i} + l_2 \hat{j} + l_3 \hat{k}$
Set up orthogonal vectors
 \hat{v}_2 & \hat{v}_3 . Arbitrarily
define $\hat{v}_2 = \hat{\lambda}_1 \times \hat{i}$
(make another choice if $\hat{\lambda}_1 = \hat{i}$).

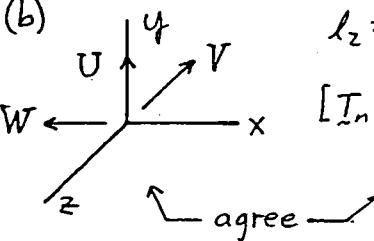
$$\hat{v}_2 = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ l_1 & l_2 & l_3 \\ 1 & 0 & 0 \end{vmatrix} = l_3 \hat{j} - l_2 \hat{k} \quad \text{Length of } \hat{v}_2 \text{ is } L_2, \quad L_2 = (l_2^2 + l_3^2)^{1/2}$$

$$\hat{v}_3 = \hat{\lambda}_1 \times \hat{v}_2 = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ l_1 & l_2 & l_3 \\ 0 & l_3 & -l_2 \end{vmatrix} = (-l_2^2 - l_3^2) \hat{i} + l_1 l_2 \hat{j} + l_1 l_3 \hat{k}$$

$$L_3 = [(-l_2^2 - l_3^2)^2 + (l_1 l_2)^2 + (l_1 l_3)^2]^{1/2}$$

Orthog. unit vectors are $\hat{\lambda}_1, \hat{v}_2/L_2, \hat{v}_3/L_3$.
At affected node n , like $[\Delta]$ in Eq. 8.1-1,

$$[\tilde{T}_n] = \begin{bmatrix} l_1 & 0 & (-l_2^2 - l_3^2)/L_3 \\ l_2 & l_3/L_2 & l_1 l_2/L_3 \\ l_3 & -l_2/L_2 & l_1 l_3/L_3 \end{bmatrix} \quad \begin{array}{l} \text{Put this in} \\ \text{matrix } [\tilde{T}] \\ \text{similar to} \\ \text{Eq. 8.4-3.} \end{array}$$

(b)  $l_2 = 1, l_1 = l_3 = 0$

$$[\tilde{T}_n] = \begin{bmatrix} 0 & 0 & -1 \\ 1 & 0 & 0 \\ 0 & -1 & 0 \end{bmatrix}$$

agree

8.4 -3

$$(a) \begin{bmatrix} AE \\ L & 0 \\ 0 & \frac{12EI}{L^3} & -\frac{6EI}{L^2} \\ 0 & -\frac{6EI}{L^2} & \frac{4EI}{L} \end{bmatrix} \begin{bmatrix} u \\ v \\ \theta \end{bmatrix} = \begin{bmatrix} 0 \\ -P \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} u \\ v \\ \theta \end{bmatrix} = \begin{bmatrix} c & -s & 0 \\ s & c & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} U \\ V \\ \Theta \end{bmatrix}$$

$c = \cos \beta$
 $s = \sin \beta$

[T]

$$\begin{bmatrix} c & s & 0 \\ -s & c & 0 \\ 0 & 0 & 1 \end{bmatrix} \underbrace{\begin{bmatrix} c \frac{AE}{L} & -s \frac{AE}{L} & 0 \\ s \frac{12EI}{L^3} & c \frac{12EI}{L^3} & -\frac{6EI}{L^2} \\ -s \frac{6EI}{L^2} & -c \frac{6EI}{L^2} & \frac{4EI}{L} \end{bmatrix}}_{[K'][T]} \quad \begin{array}{l} \text{"Omit} \\ \text{"middle"} \\ \text{in pro-} \\ \text{duct (i.e.} \\ \text{set } V=0) \end{array}$$

[T]^T [K'][T]

$$\begin{bmatrix} c^2 \frac{AE}{L} + s^2 \frac{12EI}{L^3} & -s \frac{6EI}{L^2} \\ -s \frac{6EI}{L^2} & \frac{4EI}{L} \end{bmatrix} \begin{bmatrix} U \\ \Theta \end{bmatrix} = \begin{bmatrix} -sP \\ 0 \end{bmatrix}$$

$$(b) U = -sP \left[c^2 \frac{AE}{L} + s^2 \frac{12EI}{L^3} \right]^{-1}$$

8.5-1

Substitute $\xi, \eta = \pm \frac{1}{2}$ in bilinear shape functions, Eqs. 6.2-3, e.g.

$$u_A = \frac{1}{4} \left(\frac{3}{2} \right) \left(\frac{3}{2} \right) u_1 + \frac{1}{4} \left(\frac{1}{2} \right) \left(\frac{3}{2} \right) u_2 + \frac{1}{4} \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) u_3 + \frac{1}{4} \left(\frac{3}{2} \right) \left(\frac{1}{2} \right) u_4$$

$$u_4 = \frac{1}{16} (9u_1 + 3u_2 + u_3 + 3u_4)$$

$$\begin{Bmatrix} u_A \\ u_B \\ u_C \\ v_A \\ v_B \\ v_C \end{Bmatrix} = \begin{Bmatrix} T_1 & 0 \\ 0 & T_1 \end{Bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ v_1 \\ \vdots \\ v_4 \end{Bmatrix}, \quad \text{where } [T_1] \text{ is}$$

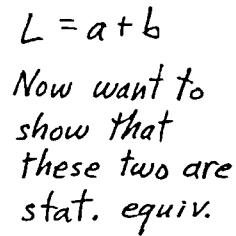
$$\frac{1}{16} \begin{bmatrix} 9 & 3 & 1 & 3 \\ 3 & 9 & 3 & 1 \\ 1 & 3 & 9 & 3 \end{bmatrix}$$

8.5-2

$$\{r\} = [I]^T \{r'\} = \frac{1}{L} \begin{bmatrix} a & 0 & c \\ 0 & a & s \\ b & 0 & -c \\ 0 & b & -s \end{bmatrix} \begin{Bmatrix} F_x \\ F_y \\ M_S \end{Bmatrix} \quad \begin{aligned} c &= \cos \beta \\ s &= \sin \beta \end{aligned}$$

↓ (result)

Free body diagram of a beam segment with length $L = a + b$. At point 1 (left), there is a vertical force $\frac{b}{L}F_y - s \frac{M_S}{L}$ and a horizontal force $\frac{b}{L}F_x - c \frac{M_S}{L}$. At point 2 (right), there is a vertical force $\frac{a}{L}F_y + s \frac{M_S}{L}$ and a horizontal force $\frac{a}{L}F_x + c \frac{M_S}{L}$.



Now want to show that these two are stat. equiv.

$$F_x = \frac{b}{L}F_y - c \frac{M_S}{L} + \frac{a}{L}F_x + c \frac{M_S}{L} = \frac{a+b}{L}F_x = F_x$$

$$F_y = \frac{b}{L}F_y - s \frac{M_S}{L} + \frac{a}{L}F_y + s \frac{M_S}{L} = \frac{a+b}{L}F_y = F_y$$

$$\begin{aligned} M_S &= bc \left(\frac{a}{L}F_x + c \frac{M_S}{L} \right) - ac \left(\frac{b}{L}F_x - c \frac{M_S}{L} \right) \\ &\quad + bs \left(\frac{a}{L}F_y + s \frac{M_S}{L} \right) - as \left(\frac{b}{L}F_y - s \frac{M_S}{L} \right) \\ &= [(a+b)c^2 + (a+b)s^2] \frac{M_S}{L} = (a+b) \frac{M_S}{L} = M_S \end{aligned}$$

8.5-3

$$u_5 = \frac{c}{L_2} u_1 + \frac{d}{L_2} u_4 \quad u_6 = \frac{a}{L_1} u_2 + \frac{b}{L_1} u_3$$

$$v_5 = \frac{c}{L_2} v_1 + \frac{d}{L_2} v_4 \quad v_6 = \frac{a}{L_1} v_2 + \frac{b}{L_1} v_3$$

$$\begin{bmatrix} u_5 & v_5 & u_6 & v_6 \end{bmatrix}^T = [T] \begin{bmatrix} u_1 & v_1 & u_2 & v_2 & u_3 & v_3 & u_4 & v_4 \end{bmatrix}^T$$

where $[T]$ is the 4 by 8 matrix

$$\begin{bmatrix} c/L_2 & 0 & 0 & 0 & 0 & 0 & d/L_2 & 0 \\ 0 & c/L_2 & 0 & 0 & 0 & 0 & 0 & d/L_2 \\ 0 & 0 & a/L_1 & 0 & b/L_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & a/L_1 & 0 & b/L_1 & 0 & 0 \end{bmatrix}$$

8.5-4

$$(a) \{\underline{d}_1\} = [\underline{I}_1]\{\underline{d}_2\}, \text{ where } [\underline{I}_1] \text{ is}$$

$$\begin{bmatrix} 1 & 0 & \underset{8 \times 1}{H/2} & \underset{8 \times 6}{0} & \underset{6 \times 1}{0} & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & H/2 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 & 0 & -H/2 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 1 & 0 & -H/2 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{l} \text{This transfor-} \\ \text{mation sets} \\ v_1 = v_4 \text{ and} \\ v_2 = v_3. \end{array}$$

$$(b) \{\underline{d}_2\} = [\underline{I}_2]\{\underline{d}_1\}, \text{ where } [\underline{I}_2] \text{ is}$$

$$\begin{bmatrix} 1/2 & 0 & 0 & 0 & 0 & 0 & 1/2 & 0 \\ 0 & 1/2 & 0 & 0 & 0 & 0 & 0 & 1/2 \\ 1/H & 0 & 0 & 0 & 0 & 0 & -1/H & 0 \\ 0 & 0 & 1/2 & 0 & 1/2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1/2 & 0 & 1/2 & 0 & 0 \\ 0 & 0 & 1/H & 0 & -1/H & 0 & 0 & 0 \end{bmatrix}$$

This transformation averages the d.o.f. at each end of el. 1 to get the translational d.o.f. of el. 2, and says $\theta_1 = \frac{v_1 - v_4}{H}$, $\theta_2 = \frac{v_2 - v_3}{H}$.

$$(c) \{\underline{d}_1\} = [\underline{I}_1]\{\underline{d}_2\} = [\underline{I}_2][\underline{I}_1]\{\underline{d}_1\}$$

$$\{\underline{d}_2\} = [\underline{I}_2]\{\underline{d}_1\} = [\underline{I}_2][\underline{I}_1]\{\underline{d}_2\}$$

Hence we expect that $[\underline{I}_1][\underline{I}_2]$ and $[\underline{I}_2][\underline{I}_1]$ are both unit matrices, but:

$$\cdots \cdots \underline{I}_{1+2+2+2} = [\underline{I}], \quad [\underline{I}_2][\underline{I}_1] = \begin{bmatrix} I \\ 0 \end{bmatrix}$$

The operation $[\underline{I}_1]\{\underline{d}_2\}$ expands 6 pieces of information to 8, and $[\underline{I}_2][\underline{I}_1]\{\underline{d}_2\}$

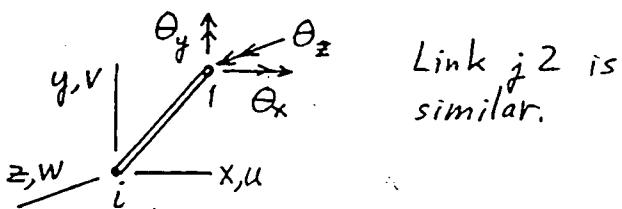
back again; nothing is lost. The operation $[\underline{I}_1][\underline{I}_2]\{\underline{d}_1\}$ condenses, then expands, but in expanding does not separate the v_i from their combination in the definition of the θ_i .

8.5-5

$$\begin{array}{c}
 \text{Diagram showing two coordinate frames } u_i \text{ and } u_j \\
 \text{Frame } u_i \text{ has axes } \theta_i^x, \theta_i^y, \theta_i^z \\
 \text{Frame } u_j \text{ has axes } \theta_j^x, \theta_j^y, \theta_j^z \\
 \text{Transformation matrix from } u_i \text{ to } u_j \\
 \text{Matrix:} \\
 \begin{bmatrix} u_i \\ w_i \\ \theta_i \end{bmatrix} = \begin{bmatrix} 1 & 0 & b_1 \\ 0 & 1 & -a_1 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} u_j \\ w_j \\ \theta_j \end{bmatrix}
 \end{array}$$

$$\begin{bmatrix} u_i \\ w_i \\ \theta_i \end{bmatrix} = \begin{bmatrix} 1 & 0 & b_1 \\ 0 & 1 & -a_1 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} u_j \\ w_j \\ \theta_j \end{bmatrix}$$

8.5-6



Link j^2 is similar.

$$[u_i \ v_i \ w_i \ \theta_{x_i} \ \theta_{y_i} \ \theta_{z_i} \ u_j \ v_j \ w_j \ \theta_{x_j} \ \theta_{y_j} \ \theta_{z_j}]^T =$$

$$\begin{bmatrix} I_1 & 0 \\ 0 & I_2 \end{bmatrix}_{12 \times 12} [u_1 \ v_1 \ w_1 \ \theta_{x_1} \ \theta_{y_1} \ \theta_{z_1} \ u_2 \ v_2 \ w_2 \ \theta_{x_2} \ \theta_{y_2} \ \theta_{z_2}]^T$$

$$[I_1]_{6 \times 6} = \begin{bmatrix} 1 & 0 & 0 & 0 & -(z_i - z_i) & (y_i - y_i) \\ 0 & 1 & 0 & (z_i - z_i) & 0 & -(x_i - x_i) \\ 0 & 0 & 1 & -(y_i - y_i) & (x_i - x_i) & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

Obtain $[I_2]$ from $[I_1]$ by changing
 i to j and 1 to 2.

8.5-7

$$(a) \quad \dot{\theta} = \frac{u_3 - u_2}{b} \quad v_1 = v_3 + \theta a$$

$$\begin{Bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \end{Bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ -a/b & a/b & 1 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u_2 \\ u_3 \\ v_3 \end{Bmatrix}$$

$$v_2 = v_3$$

$$u_1 = u_3$$

$$(b) \quad \dot{\theta} = \frac{u_2 - u_1}{y_1 - y_2} \quad (\text{OK if } y_1 \neq y_2)$$

Relative to node 1,

$$v_2 = \theta(x_2 - x_1)$$

$$u_3 = -\theta(y_3 - y_1)$$

$$v_3 = \theta(x_3 - x_1)$$

$$\begin{Bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \end{Bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \\ -(x_2 - x_1)\alpha & 1 & (x_2 - x_1)\alpha \\ 1 + (y_3 - y_1)\alpha & 0 & -(y_3 - y_1)\alpha \\ -(x_3 - x_1)\alpha & 1 & (x_3 - x_1)\alpha \end{bmatrix} \begin{Bmatrix} u_1 \\ v_1 \\ u_2 \end{Bmatrix}$$

three master d.o.f.

$$\text{Let } \alpha = \frac{1}{y_1 - y_2}$$

8.6-1

Along AB Apply $\{\sigma\} = [\underline{E}] \{\epsilon\}$
with $\epsilon_x = u_{,x}$, etc.

$$\sigma_x = -P, \text{ so } -P = \frac{E}{1-\nu^2} (u_{,x} + \nu v_{,y})$$

$$T_{xy} = 0, \text{ so } 0 = u_{,y} + v_{,x}$$

These are 2 constraint eqs. on 4 d.o.f.

Along CD Same as AB, except $P = 0$.

Along AD Can transform d.o.f. to the
st axes by use of Eqs. 8.1-3 & 8.2-3;
then treat like edge CD.

Along BC $u = v = u_{,x} = v_{,x} = 0$. But $u_{,y}$
& $v_{,y}$ are unknown, as are corresp.
terms in $\{R\}$. Can perhaps set these
load terms to zero with little consequence

Anisotropy E.g. along AB,

$$\begin{Bmatrix} -P \\ \sigma_y \\ 0 \end{Bmatrix} = [\underline{E}] \begin{Bmatrix} \epsilon_x \\ \epsilon_y \\ \gamma_{xy} \end{Bmatrix} \quad \text{From the 1st \& 3rd
of these equations,}$$

$$\begin{aligned} -P &= E_{11} u_{,x} + E_{12} v_{,y} + E_{13} (u_{,y} + v_{,x}) \\ 0 &= E_{31} u_{,x} + E_{32} v_{,y} + E_{33} (u_{,y} + v_{,x}) \end{aligned} \quad \left. \begin{array}{l} \text{2 constraint} \\ \text{eqs.} \end{array} \right\}$$

8.6-2

(a) Use the beam N_i of Fig. 3.2-4:

$$\underline{u} = [N_1 \ N_2 \ N_3 \ N_4] [u_1 \ \epsilon_{x_1} \ u_2 \ \epsilon_{x_2}]^T$$

$[\underline{B}] = \frac{d}{dx} [\underline{N}]$, etc. However, it is easier to use the "a-basis", $\underline{u} = [1 \ x \ x^2 \ x^3] \{\underline{a}\}$

$$[\underline{k}_a] = \int_0^L [\underline{B}_a]^T [\underline{B}_a] A E dx, \text{ where } [\underline{B}_a] =$$

$$[0 \ 1 \ 2x \ 3x^2], [\underline{k}] = [\underline{A}]^{-T} [\underline{k}_a] [\underline{A}]^{-1}$$

and $[\underline{A}]^{-1}$ is computed in Prob. 3.2-4

$$AE \underbrace{\begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & L & L^2 & L^3 \\ 0 & L^2 & \frac{4}{3}L^3 & \frac{3}{2}L^4 \\ 0 & L^3 & \frac{3}{2}L^4 & \frac{9}{5}L^5 \end{bmatrix}}_{[\underline{k}_a]}, AE \underbrace{\begin{bmatrix} 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ -L & -\frac{L^2}{6} & L & \frac{L^2}{6} \\ -9L^2 & -2L^3 & 9L^2 & 3L^3 \end{bmatrix}}_{[\underline{k}_a][\underline{A}]^{-1}}$$

$$\underbrace{\begin{bmatrix} 1 & 0 & -3/L^2 & 2/L^3 \\ 0 & 1 & -2/L & 1/L^2 \\ 0 & 0 & 3/L^2 & -2/L^3 \\ 0 & 0 & -1/L & 1/L^2 \end{bmatrix}}_{[\underline{A}]^{-T}}, \underbrace{\begin{bmatrix} 36 & 3L & -36 & 3L \\ 3L & 4L^2 & -3L & -L^2 \\ -36 & -3L & 36 & -3L \\ 3L & -L^2 & -3L & 4L^2 \end{bmatrix}}_{[\underline{k}]}$$

$$(b) \begin{array}{c} \xrightarrow{\hspace{2cm}} \\ \xleftarrow{\hspace{2cm}} \end{array} \quad u_1 = 0, \text{ so } \frac{AE}{30L} \begin{bmatrix} 4L^2 & -3L & -L^2 \\ -3L & 36 & -3L \\ -L^2 & -3L & 4L^2 \end{bmatrix} \begin{Bmatrix} \epsilon_{x_1} \\ u_2 \\ \epsilon_{x_2} \end{Bmatrix} = \begin{Bmatrix} 0 \\ P \\ F_{x_2} \end{Bmatrix}$$

$$\text{now impose } \epsilon_{x_2} = \frac{P}{AE} : \frac{AE}{30L} \begin{bmatrix} 4L^2 & -3L & 0 \\ -3L & 36 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} \epsilon_{x_1} \\ u_2 \\ \epsilon_{x_2} \end{Bmatrix} = \begin{Bmatrix} (AE/30L)L^2(P/AE) \\ P + (AE/30L)3L(P/AE) \\ P/AE \end{Bmatrix}$$

... from the first two equations, inverting the 2 by 2 matrix,

$$\begin{Bmatrix} \epsilon_{x_1} \\ u_2 \end{Bmatrix} = \frac{30L}{AE} \frac{1}{135L^2} \begin{bmatrix} 36 & 3L \\ 3L & 4L^2 \end{bmatrix} \begin{Bmatrix} PL/30 \\ 1.1P \end{Bmatrix} = \frac{1}{4.5AE} \begin{Bmatrix} 1.2PL + 3.3PL \\ 0.1PL^2 + 4.4PL^2 \end{Bmatrix}$$

$$\begin{Bmatrix} \epsilon_{x_1} \\ u_2 \end{Bmatrix} = \begin{Bmatrix} P/AE \\ PL/AE \end{Bmatrix} \quad \checkmark$$

8.7-1

$$J = \lfloor N_{\xi} \rfloor \{ \tilde{x} \}$$

$$J = \left[-\frac{1+2\xi}{2} \quad -2\xi \quad \frac{1+2\xi}{2} \right] \begin{Bmatrix} 0 \\ L/3 \\ L \end{Bmatrix} = \frac{L}{3} \left(\frac{3}{2} + \xi \right)$$

$$J=0 \text{ at } \xi = -\frac{3}{2}$$

$$x = L \lfloor N_{\xi} \rfloor \{ \tilde{x} \} = \left[\frac{-\xi + \xi^2}{2} \quad 1 - \xi^2 \quad \frac{\xi + \xi^2}{2} \right] \begin{Bmatrix} 0 \\ L/3 \\ L \end{Bmatrix} = \frac{L}{3} \left(1 + \frac{3}{2} \xi + \frac{1}{2} \xi^2 \right)$$

$$\text{For } \xi = -\frac{3}{2}, \quad x = \frac{L}{3} \left(1 - \frac{9}{4} + \frac{9}{8} \right) = -\frac{L}{24}, \quad \text{so} \quad \frac{x}{L} = -0.04167$$

8.8-1

(a) From Eqs. 3.2-3 and 3.2-8,

$$v = \begin{bmatrix} x \\ \vdots \\ x^3 \end{bmatrix} [A]^{-1} \{d\} \quad \text{Hence}$$

$$[k_f] = \beta [A]^{-T} \underbrace{\left(\int_0^L \begin{bmatrix} 1 & x & x^2 & x^3 \end{bmatrix} \begin{bmatrix} 1 & x & x^2 & x^3 \end{bmatrix}^T b dx \right)}_{b = \text{width of the beam}} [A]^{-1}$$

$$\begin{bmatrix} L & L^2/2 & L^3/3 & L^4/4 \\ L^3/3 & L^4/4 & L^5/5 & \vdots \\ \vdots & \vdots & \vdots & \vdots \\ \text{symm.} & L^5/5 & L^6/6 & L^7/7 \end{bmatrix} b = \begin{bmatrix} g \\ \vdots \\ g \end{bmatrix}. \quad \text{Hence,}$$

$$\frac{\beta b L}{420} \begin{bmatrix} 156 & 22L & 54 & -13L \\ 4L^2 & 13L & -3L^2 & \vdots \\ \vdots & \vdots & \vdots & \vdots \\ \text{symm.} & 156 & -22L & 4L^2 \end{bmatrix} [k_f] = \beta [A]^{-T} \begin{bmatrix} g \\ \vdots \\ g \end{bmatrix} [A]^{-1}$$

$$(b) v = \underbrace{\begin{bmatrix} \frac{L-x}{L} & \frac{(L-x)x}{2L} & \frac{x}{L} & -\frac{(L-x)x}{2L} \end{bmatrix}}_{LN} \begin{Bmatrix} v_1 \\ \theta_1 \\ v_2 \\ \theta_2 \end{Bmatrix}$$

$$[k_f] = \beta \int_0^L [LN]^T [LN] b dx \quad \text{After tedious expansion \& integration,}$$

$$[k_f] = \frac{\beta b L}{120} \begin{bmatrix} 40 & 5L & 20 & -5L \\ L^2 & 5L & -L^2 & \vdots \\ \vdots & \vdots & \vdots & \vdots \\ \text{symm.} & 40 & -5L & L^2 \end{bmatrix} \begin{Bmatrix} v_1 \\ \theta_1 \\ v_2 \\ \theta_2 \end{Bmatrix}$$

$$(c) v = \begin{bmatrix} \frac{-x}{L} & \frac{x}{L} \end{bmatrix} \begin{Bmatrix} w_1 \\ w_2 \end{Bmatrix} = LN \begin{Bmatrix} v_1 \\ v_2 \end{Bmatrix}$$

$$[k_f] = \beta \int_0^L [LN]^T [LN] b dx = \frac{\beta b L}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix} \begin{Bmatrix} v_1 \\ v_2 \end{Bmatrix}$$

(Can include θ_1 & θ_2 by adding zeros to $[k_f]$)

(d) Rigid body motion; gives diagonal $[k_f]$.

For $\{d\} = [v_1 \ \theta_1 \ v_2 \ \theta_2]^T$,

$$[k_f] = \frac{\beta b L}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \end{bmatrix}$$

All these formulations are valid; that is,
all provide correct convergence with
mesh refinement

8.8-2

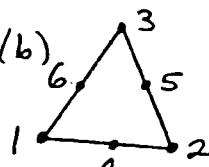


In area coords.,
 $w = [\xi_1 \ \xi_2 \ \xi_3] \begin{Bmatrix} w_1 \\ w_2 \\ w_3 \end{Bmatrix}$

$$[k_f] = \int \begin{Bmatrix} \xi_1^2 & \xi_1 \xi_2 & \xi_1 \xi_3 \\ \xi_1 \xi_2 & \xi_2^2 & \xi_2 \xi_3 \\ \xi_1 \xi_3 & \xi_2 \xi_3 & \xi_3^2 \end{Bmatrix} dA$$

Integrate by use of Eq. 7.3-7.

(b)


 $[k_f] = \frac{\beta A}{12} \begin{Bmatrix} 2 & 1 & 1 \\ 1 & 2 & 1 \\ 1 & 1 & 2 \end{Bmatrix}$
 $w = [N_i] \begin{Bmatrix} w_1 \\ w_2 \\ w_3 \\ w_4 \\ w_5 \\ w_6 \end{Bmatrix}$

N_i given by Eq. 7.3-4.
 Integrate by use of Eq. 7.3-7.

For $i=1, 2, 3$, $\int_A N_i^2 dA = \frac{A}{30}$

For i or $j=1, 2, 3$ but $i \neq j$, $\int_A N_i N_j dA = -\frac{A}{180}$

For $i=4, 5, 6$, $\int_A N_i^2 dA = \frac{8A}{45}$

For i or $j=4, 5, 6$ but $i \neq j$, $\int_A N_i N_j dA = \frac{4A}{45}$

$\int_A N_1 N_5 dA = \int_A N_2 N_6 dA = \int_A N_3 N_4 dA = -\frac{A}{45}$

integrals of $N_1 N_4$, $N_1 N_6$, $N_2 N_4$, $N_2 N_5$,
 $N_3 N_5$, and $N_3 N_6$ are zero. Hence

$$[k_f] = \frac{1}{180} \begin{Bmatrix} 6 & -1 & -1 & 0 & -4 & 0 \\ -1 & 6 & -1 & 0 & 0 & -4 \\ 1 & -1 & 6 & -4 & 0 & 0 \\ 0 & 0 & -4 & 32 & 16 & 16 \\ -4 & 0 & 0 & 16 & 32 & 16 \\ 0 & -4 & 0 & 16 & 16 & 32 \end{Bmatrix}$$

8.8-3

Strain energy per unit of area A is

$$dU = \frac{\beta}{2} w dA (w) + \frac{\alpha}{2} w_x dA (w_x) + \frac{\alpha}{2} w_y dA (w_y)$$

where $\beta w dA$ = force $\alpha w_x dA$ = moment
 w = deflection w_x = rotation

Hence

$$U = \frac{1}{2} \int_A [w \ w_x \ w_y] \begin{bmatrix} \beta \\ \alpha \\ \alpha \end{bmatrix} \begin{bmatrix} w \\ w_x \\ w_y \end{bmatrix} dA$$

Let $[w \ w_x \ w_y]^T = [\underline{Q}] \{\underline{d}\}$. Then

$$[\underline{k}_f]_{n \times n} = \int_A [\underline{Q}]^T [\beta \ \alpha \ \alpha] [\underline{Q}] dA$$

8.8-4

$$(a) \text{ Subs. } \xi = 1 - \frac{2a}{r} \text{ into } \phi = \frac{1}{2}(1-\xi)\phi_1 + \frac{1}{2}(1+\xi)\phi_3$$

$$\phi = \left(\frac{1}{2} - \frac{1}{2} + \frac{a}{r}\right)\phi_1 + \left(\frac{1}{2} + \frac{1}{2} - \frac{a}{r}\right)\phi_3 = \frac{a}{r}\phi_1 + \left(1 - \frac{a}{r}\right)\phi_3$$

$$\phi = c \text{ if } \phi_1 = \phi_3 = c, \quad \phi \rightarrow \phi_3 \text{ as } r \rightarrow \infty$$

(b) From Eq. 8.8-3,

$$J = \frac{\partial x}{\partial \xi} = \frac{(1-\xi)(-2) - (-2\xi)(-1)}{(1-\xi)^2} x_1 + \frac{(1-\xi)(1) - (1+\xi)(-1)}{(1-\xi)^2} x_2$$

$$J = \frac{-2}{(1-\xi)^2} x_1 + \frac{2}{(1-\xi)^2} x_2 = \frac{2(x_2 - x_1)}{(1-\xi)^2} = \frac{2a}{(1-\xi)^2}$$

$$(c) [B] = \frac{1}{J} \frac{d}{d\xi} \begin{bmatrix} 1-\xi & 1+\xi \\ 2 & 2 \end{bmatrix} = \frac{(1-\xi)^2}{4a} \begin{bmatrix} -1 & 1 \end{bmatrix}$$

$$[k] = \int_{-1}^1 [B]^T E [B] J A d\xi = \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \frac{EA}{16a^2} 2a \int_{-1}^1 (1-\xi)^2 d\xi$$

$$[k] = \frac{EA}{8a} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \frac{8}{3} = \frac{EA}{3a} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

8.8-5

$$(a) \quad \phi = L \begin{Bmatrix} N_1 \\ N_2 \\ N_3 \\ N_4 \end{Bmatrix} \begin{Bmatrix} \phi_1 \\ \phi_2 \\ \phi_5 \\ \phi_6 \end{Bmatrix}$$

$$N_1 = \frac{1}{4}(1-\xi)(1-\eta)$$

$$N_2 = \frac{1}{4}(1-\xi)(1+\eta) \quad \text{Mapping functions}$$

$$N_3 = \frac{1}{4}(1+\xi)(1-\eta) \quad M_i \text{ same as in}$$

$$N_4 = \frac{1}{4}(1+\xi)(1+\eta) \quad \text{Fig. 8.8-4.}$$

(b) Using derivatives of M_i in Fig. 8.8-4,

$$[\underline{\underline{J}}] = \begin{bmatrix} -2 & \frac{1-\eta}{2} & -2 & \frac{1+\eta}{2} & \frac{2}{(1-\xi)^2} & \frac{1-\eta}{2} & \frac{2}{(1-\xi)^2} & \frac{1+\eta}{2} \\ \frac{\xi}{(1-\xi)^2} & 2 & \frac{-\xi}{(1-\xi)^2} & 2 & \frac{1-\xi}{2} & 2 & \frac{1+\xi}{2} & 2 \end{bmatrix} \begin{bmatrix} a & 0 \\ a & 2b \\ 2a & 0 \\ 2a & 2b \end{bmatrix}$$

$$[\underline{\underline{J}}] = \begin{bmatrix} \frac{a}{(1-\xi)^2} & 0 \\ 0 & b \end{bmatrix}, \quad J = \frac{ab}{(1-\xi)^2}$$

$$(c) \quad [\underline{\underline{B}}] = \begin{bmatrix} N_1, x \\ N_1, y \end{bmatrix} = [\underline{\underline{J}}]^{-1} \begin{bmatrix} N_1, x \\ N_1, y \end{bmatrix} \quad \text{with only } \phi_1 \text{ & } \phi_2 \text{ active.}$$

$$[\underline{\underline{B}}] = \frac{(1-\xi)^2}{ab} \begin{bmatrix} b & 0 \\ 0 & \frac{a}{(1-\xi)^2} \end{bmatrix} \frac{1}{4} \begin{bmatrix} -(1-\eta) & -(1+\eta) \\ -(1-\xi) & (1-\xi) \end{bmatrix}$$

$$[\underline{\underline{B}}] = \frac{(1-\xi)^2}{4ab} \begin{bmatrix} -b(1-\eta) & -b(1+\eta) \\ -\frac{a}{1-\xi} & \frac{a}{1-\xi} \end{bmatrix}$$

$$[\underline{\underline{k}}] = \int_{-1}^1 \int_{-1}^1 [\underline{\underline{B}}]^T k [\underline{\underline{B}}] t J d\xi d\eta$$

$$[\underline{\underline{k}}] = \frac{n}{16ab} \left| \int_{-1}^1 \int_{-1}^1 \begin{bmatrix} b^2(1-\xi)^2(1-\eta)^2 + a^2 \\ b^2(1-\xi)^2(1-\eta^2) - a^2 \\ b^2(1-\xi)^2(1-\eta^2) - a^2 \\ b^2(1-\xi)^2(1+\eta)^2 + a^2 \end{bmatrix} d\xi d\eta \right|$$

$$\int_{-1}^1 (1+\eta^2) d\eta = \frac{8}{3}$$

$$\int_{-1}^1 (1-\eta^2) d\eta = \frac{4}{3}$$

$$[\underline{\underline{k}}] = \frac{kt}{16Ab} \begin{bmatrix} \frac{64}{9}b^2 + 2a^2 & \frac{32}{9}b^2 - 2a^2 \\ \frac{32}{9}b^2 - 2a^2 & \frac{64}{9}b^2 + 2a^2 \end{bmatrix}$$

8.8-6

$$M_1 = -\frac{2\bar{s}}{1-\bar{s}} \frac{-\eta+\eta^2}{2} \quad M_4 = \frac{1+\bar{s}}{1-\bar{s}} \frac{-\eta+\eta^2}{2}$$

$$M_2 = -\frac{2\bar{s}}{1-\bar{s}} (1-\eta^2) \quad M_5 = \frac{1+\bar{s}}{1-\bar{s}} (1-\eta^2)$$

$$M_3 = -\frac{2\bar{s}}{1-\bar{s}} \frac{\eta+\eta^2}{2} \quad M_6 = \frac{1+\bar{s}}{1-\bar{s}} \frac{\eta+\eta^2}{2}$$

$$(a) \underline{K}^* = \underline{K} + \Delta \underline{K}, \Delta \underline{K} = K^* - K = 0.3$$

$$\text{Iterative eq. is } 0.5 D_{i+1}^* = 2 - 0.3 D_i^*$$

$$\text{i.e. } D_{i+1}^* = 4 - 0.6 D_i^*$$

$$D_2^* = 4 - 0.6(4) = 1.6 \quad \begin{matrix} \text{Converges} \\ \text{to } D^* = \end{matrix}$$

$$D_3^* = 4 - 0.6(1.6) = 3.04$$

$$D_4^* = 4 - 0.6(3.04) = 2.176 \quad \begin{matrix} 2.50, \text{ i.e.} \\ \text{to exact} \end{matrix}$$

$$D_5^* = 4 - 0.6(2.176) = 2.6944$$

$$D_6^* = 4 - 0.6(2.6944) = 2.38336 \quad \begin{matrix} \text{value.} \\ \text{to exact} \end{matrix}$$

$$(b) D_{i+1}^* = \frac{1}{k}(R - \Delta k D_i^*) = D - \frac{\Delta k}{k} D_i^*$$

$$D_2^* = D - \frac{\Delta k}{k} D$$

$$D_3^* = D - \frac{\Delta k}{k} D_2^* = D - \frac{\Delta k}{k} D + \left(\frac{\Delta k}{k}\right)^2 D$$

$$D_4^* = D - \frac{\Delta k}{k} D_3^* = D \left[1 - \frac{\Delta k}{k} + \left(\frac{\Delta k}{k}\right)^2 - \left(\frac{\Delta k}{k}\right)^3 \right]$$

etc., so the series in brackets extends.

The series converges if $\left|\frac{\Delta k}{k}\right| < 1$.

Hence, magnitude of increase or decrease in k must be less than 100%.