

Figure 2. Normalized low-pass requirements.

at least  $A_s$  dB. In the passbands (below  $f_1$  Hz and above  $f_2$  Hz), the maximum attenuation is  $A_p$  dB. The bands from  $f_1$  to  $f_3$  and from  $f_4$  to  $f_2$  are called the *transition bands*. The filter requirement is said to be geometrically symmetrical if  $f_1 f_2 = f_3 f_4$ .

An approach to designing a circuit (a band-stop filter) with a frequency response that satisfies the band-stop requirements shown in Fig. 1 is described below. It consists of two steps: the approximation of the requirements by a transfer function, and the synthesis of the transfer function.

In the approximation part of the design process, it is desirable to find a transfer function with a frequency response that satisfies the band-stop requirements. To find that transfer function, first convert the band-stop requirements into the normalized low-pass requirements. For the case that the band-stop requirements are symmetrical, the corresponding normalized low-pass requirements are shown in Fig. 2. The normalized passband frequency  $F_p = 1$  and the passband attenuation is  $A_p$  dB. The normalized stopband frequency is

$$F_s = \frac{f_2 - f_1}{f_4 - f_3}$$

and the stopband attenuation is  $A_s$  dB.

With such low-pass requirements, we can obtain the corresponding low-pass transfer function  $T_{LP}(s)$ . (See LOW-PASS FILTERS for more information about how to obtain the transfer function.) The band-stop filter transfer function  $T_{BS}(s)$  is obtained by making the transformation

$$T_{BS}(s) = T_{LP}(s) \Big|_{s = \frac{Bs}{s^2 + (2\pi f_0)^2}}$$

where  $B$  is the bandwidth of the band-stop filter defined as

$$B = 2\pi(f_2 - f_1)$$

and  $f_0$  is the center frequency of the band-stop requirement defined as

$$f_0 = \sqrt{f_1 f_2} = \sqrt{f_3 f_4}$$

To use this method when the requirement is not symmetrical, for the case that  $f_1 f_2 > f_3 f_4$ , we form a more stringent requirement by either decreasing  $f_2$  or increasing  $f_4$ , so that the symmetrical condition is met. The band-stop transfer function that satisfies the new requirements must also satisfy

## BAND-STOP FILTERS

A band-stop filter (also known as band-reject, band-elimination, or notch filter) suppresses a band of frequencies of a signal, leaving intact the low- and high-frequency bands. A band-stop filter specification can be expressed as shown in Fig. 1. In the stopband from  $f_3$  Hz to  $f_4$  Hz, the attenuation is

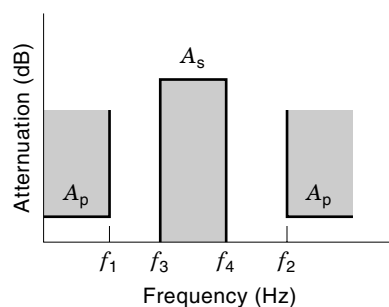


Figure 1. Band-stop filter specification.

the original requirements. In case  $f_1 f_2 < f_3 f_4$ , we either increase  $f_1$  or decrease  $f_3$  and then apply the same procedure.

A simple example is provided to illustrate this concept. For the band-stop requirements  $A_s = 25$  dB,  $A_p = 3.01$  dB,  $f_1 = 1$  kHz,  $f_2 = 100$  kHz,  $f_3 = 8$  kHz, and  $f_4 = 12.5$  kHz; the corresponding normalized low-pass requirements are:  $A_s = 25$  dB,  $A_p = 3.01$  dB,  $F_p = 1$ , and  $F_s = 22$ . Choosing a single-pole Butterworth approximation, the low-pass transfer function for the normalized low-pass requirements is

$$T_{LP}(s) = \frac{1}{s + 1}$$

which meets the stopband requirements easily. The band-stop transfer function is obtained by the transformation

$$T_{BS}(s) = \frac{1}{S + 1} \Bigg|_{S = \frac{2\pi(100 \times 10^3 - 1 \times 10^3)s}{s^2 + (2\pi 100 \times 10^3)(2\pi 1 \times 10^3)}}$$

which simplifies to

$$T_{BS}(s) = \frac{s^2 + 3.948 \times 10^9}{s^2 + 6.220 \times 10^5 s + 3.948 \times 10^9}$$

Note that the single-pole low-pass function has been transformed to a two-pole band-stop function. The above band-stop transfer function is in the so called biquadratic form, which is an expression of the form

$$\frac{s^2 + a_1 + a_2}{s^2 + b_1 s + b_2} \quad (1)$$

There are a number of ways to synthesize and biquadratic function as an active network, such as the Friend biquad circuit (1,5), the Boctor circuit (2), and the summing four-amplifier biquad circuit (3,5). The Friend or Boctor circuit uses one operational amplifier. The summing four-amplifier biquad circuit is much easier to tune. When  $a_1 = 0$ , the Bainter circuit can be used. The Bainter circuit (4) is shown in Fig. 3. For higher performance circuits, see Ref. 5 for the description of different band-stop circuit topologies.

The transfer function is

$$\frac{V_{out}(s)}{V_{in}(s)} = \frac{s^2 + \frac{R_{12}}{R_{11}R_{21}R_{31}C_1C_2}}{s^2 + \left(\frac{1}{R_{31}C_1} + \frac{1}{R_{32}C_1}\right)s + \frac{1}{R_{22}R_{31}C_1C_2}}$$

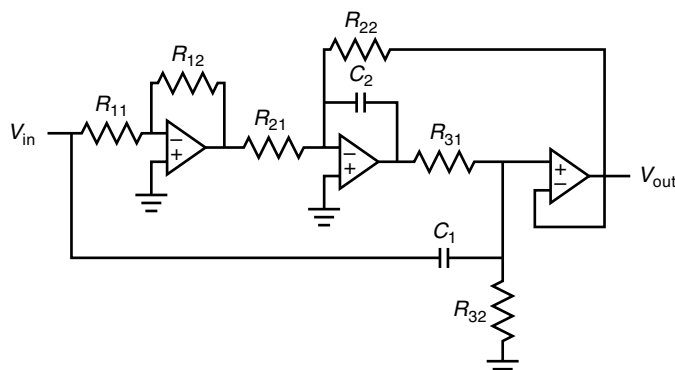


Figure 3. Bainter circuit.

Compare with Eq. (1),

$$a_1 = 0, \quad a_2 = \frac{R_{12}}{R_{11}R_{21}R_{31}C_1C_2},$$

$$b_1 = \frac{1}{R_{31}C_1} + \frac{1}{R_{32}C_1}, \quad b_2 = \frac{1}{R_{22}R_{31}C_1C_2}$$

Choose  $C_1 = C_2 = 1$ ,  $R_{12}/R_{11} = K$ ,  $R_{31} = R_{32}$ . Solving for the other values,

$$R_{21} = \frac{Kb_1}{2a_2}, \quad R_{22} = \frac{b_1}{2b_2}, \quad R_{31} = \frac{2}{b_1}$$

The impedance scaling method can be used to scale the values of  $R$  and  $C$  into the practical ranges. In general, a higher-order band-stop transfer function can be factorized into a product of biquadratic functions. Each of the biquadratic function can be synthesized by using the Bainter or other circuits. By cascading all the circuits together, the band-stop filter is realized.

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